## AMENDMENTS TO THE SPECIFICATION

Please indent the second full paragraph on page 2, line 12.

Please replace the first full paragraph on page 3, starting on line 2, with the following rewritten paragraph:

--According to the above disclosures, since the aging resistance cannot be sufficiently ensured, quenching is needed after annealing the steel in order to ensure the aging resistance. However, in this case, there is a problem in that the quenching is usually performed as a water quench in a water bath, creating an oxidized coat on the steel sheet, and is thus accompanied with pickling in order to remove the oxidized coat, thereby causing the surface defects on the steel sheet, which require additional manufacturing costs. Moreover, the steel sheet has a low strength. Additionally, since the steel sheet has poor in-plane anisotropy, creating wrinkles and ears on the steel sheet, the method suffers from large material consumption.--

Please amend the section heading at page 5, line 13, as follows:

--~~Disclosure~~ Summary of the Invention--

Please replace the first full paragraph on page 6, line 1, with the following rewritten paragraph:

--In accordance with the present invention, the above and other objects can be accomplished by the provision of a cold rolled steel sheet, comprising in weight %: 0.003 % or less of C; 0.003 ~ 0.03 % of S; 0.01 ~ 0.1 % of Al; 0.02 % or less of N; 0.2 % or less of P; at least one of 0.03 ~ 0.2 % of Mn and 0.005 ~ 0.2 % of Cu; and the balance of Fe and other unavoidable impurities, ~~in terms of weight%,~~ wherein, when the steel sheet comprises one of Mn and Cu, the composition of Mn, Cu, and S satisfies one of the relationships: $0.58*Mn/S \leq 10$ and $1 \leq 0.5*Cu/S \leq 10$, and when the steel sheet comprises both Mn and Cu, the composition of Mn, Cu, and S satisfies the relationships: $Mn+Cu \leq 0.3$ and $2 \leq 0.5*(Mn+Cu)/S \leq 20$, and wherein precipitates of MnS, CuS, and (Mn, Cu)S have an average size of 0.2 $\mu$m or less. As used above and throughout the specification and claims, the asterisk symbol "*" used in the Mn, Cu and S relationships is a symbol for multiplication.--

Please amend the section heading on page 10, line 13, as follows:

--~~Best Mode for Carrying Out the Invention~~Detailed Description of the Invention--

Please amend the section heading on page 13, line 23, as follows:

--~~[~~**Cold rolled steel sheet of the invention**~~]~~--

Please replace the paragraph on pages 19 and 20 with the following rewritten paragraph:

-- In this case, it is desirable that the precipitates are distributed in the number of $2 \times 10^6$ precipitates/$mm^2$ or more. Starting from 7 as the value of 0.5*(Mn+Cu)/S, the sorts of precipitates and the number of the precipitates are remarkably varied. Specifically, when the value of 0.5*(Mn+Cu)/S is 7 or less, lots of very fine MnS and CuS separate precipitates are uniformly distributed rather that the (Mn, Cu)S complex precipitates. Meanwhile, when the value of 0.5*(Mn+Cu)/S is more than 7, regardless of a low difference between the sizes of the precipitates, the number of precipitates distributed in the crystal grain and grain boundary is decreased because of an increased amount of the (Mn, Cu)S complex precipitates. In the present invention, an increase in the number of the precipitates can enhance the aging resistance, the in-plane anisotropy index, and the secondary work embrittlement resistance. For this purpose, the precipitates are preferably distributed in the number of $2 \times 10^8$ or more. In the present invention, even in the case where the values of 0.5*(Mn+Cu)/S are the same, a smaller amount of Mn and Cu added can reduce the number of precipitates distributed in the crystal grain and grain boundary. If the content of Mn and Cu is increased, the precipitates become coarse, leading to a reduction in the number of precipitates distributed in the crystal grain and grain boundary. --

Please amend the section heading on page 22, line 14, as follows:

--~~[~~**Method of manufacturing cold rolled steel sheet**~~]~~--

Please amend the section heading on page 22, line 23, as follows:

--~~[~~Hot rolling conditions~~]~~--

Please amend the section heading on page 26, line 5, as follows:

--~~{~~Coiling conditions~~}~~--

Please amend the section heading on page 26, line 11, as follows:

--~~{~~Cold rolling conditions~~}~~--

Please amend the section heading on page 26, line 21, as follows:

--~~{~~Continuous annealing~~}~~--

Please amend the example on page 28, line 3, as follows:

--~~{~~Example 1-1~~}~~:-MnS-precipitated steel--

Please amend the example on page 31, lines 19 and 20, as follows:

--~~{~~Example 1-2~~}~~:–High strength CuS-precipitated steel with solid solution strengthening--

Please amend the example on page 34, line 19, as follows:

--~~{~~Example 1-3~~}~~:—MnS-precipitated steel with AlN precipitation strengthening--

Please amend the example on page 36, line 7, as follows:

--~~{~~Example 2-1~~}~~:-CuS-precipitated steel--

Please amend the example on page 39, lines 4 and 5, as follows:

--~~{~~Example 2-2~~}~~–:High strength CuS-precipitated steel with solid solution strengthening--

Please amend the example on page 42, lines 6 and 7, as follows:

--~~{~~Example 2-3~~}~~–:High strength CuS-precipitated steel with AlN precipitation strengthening--

Please amend the example on page 44, line 5, as follows:

--~~[~~Example 3-1~~]~~:MnCu-precipitated steel--

Please amend the example on page 46, lines 5 and 6, as follows:

--~~[~~Example 3-2~~]~~:High strength MnCu-precipitated steel with solid solution strengthening--

Please amend the example on page 50, lines 6 and 7, as follows:

--~~[~~Example 3-3~~]~~:High strength MnCu-precipitated steel with AlN precipitation strengthening--